# **Chapter 2 Maxwell's Equations and Plane EM Waves**

#### 2-1 Dielectric and Conductor

**Displacement vector:**  $\overrightarrow{D} = \varepsilon_0 \overset{\rightarrow}{E} + \overset{\rightarrow}{P} = \varepsilon \overset{\rightarrow}{E} = \varepsilon_0 (1 + \chi_e) \overset{\rightarrow}{E} = \varepsilon_0 \varepsilon_r \overset{\rightarrow}{E}$ 



**Polarization vector:**  $\overrightarrow{P} = \lim_{\Delta \nu \to 0} \frac{\sum_{k=1}^{\infty} P_k}{\Delta \nu}$ 

$$V = \frac{1}{4\pi\varepsilon_0} \iiint_{v} \frac{\overrightarrow{P} \cdot \overrightarrow{a_R}}{R^2} dv',$$

$$R^{2} = (x - x')^{2} + (y - y')^{2} + (z - z')^{2}, \quad \nabla' = \stackrel{\wedge}{x} \frac{\partial}{\partial x'} + \stackrel{\wedge}{y} \frac{\partial}{\partial y'} + \stackrel{\wedge}{z} \frac{\partial}{\partial z'} \Rightarrow \nabla' \left(\frac{1}{R}\right) = \frac{\stackrel{\wedge}{a_{R}}}{R^{2}}$$

$$\Rightarrow V = \frac{1}{4\pi\varepsilon_{0}} \iiint_{v'} \overrightarrow{P} \cdot \nabla' \left(\frac{1}{R}\right) dv' = \frac{1}{4\pi\varepsilon_{0}} \left[\iiint_{v'} \nabla' \cdot \left(\frac{\overrightarrow{P}}{R}\right) dv' - \iiint_{v'} \frac{\nabla' \cdot \overrightarrow{P}}{R} dv'\right]$$

$$= \frac{1}{4\pi\varepsilon_{0}} \left[\iint_{s'} \frac{\overrightarrow{P} \cdot \stackrel{\wedge}{a_{n}}}{R} d\overrightarrow{S}' + \iiint_{v'} \frac{-\nabla' \cdot \overrightarrow{P}}{R} dv'\right]$$

Surface charge density:  $\rho_{\rm ps} = \overrightarrow{P} \cdot \overset{\wedge}{a_n}$ .

Volume charge density:  $\rho_p = -\nabla \cdot \overrightarrow{P}$ 

Total charge:  $Q = \iint_{S'} \overrightarrow{P} \cdot \overrightarrow{a_n} \ d\overrightarrow{S'} + \iiint_{V'} \nabla \cdot \overrightarrow{P} \ dv' = 0$ 

$$\nabla \cdot \overrightarrow{E} = \frac{1}{\varepsilon_0} \left( \rho + \rho_p \right) \implies \nabla \cdot \left( \varepsilon_0 \overrightarrow{E} + \overrightarrow{P} \right) = \rho$$

Define  $\overrightarrow{D} = \varepsilon_0 \overrightarrow{E} + \overrightarrow{P} \implies \nabla \cdot \overrightarrow{D} = \rho \iff \iint_s \overrightarrow{D} \cdot d\overrightarrow{S} = Q$ 

Note: Generally,  $\overrightarrow{D} = \stackrel{\leftrightarrow}{\varepsilon} \cdot \stackrel{\rightarrow}{E}$  or  $\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \begin{bmatrix} \varepsilon_{11} & \varepsilon_{12} & \varepsilon_{13} \\ \varepsilon_{21} & \varepsilon_{22} & \varepsilon_{23} \\ \varepsilon_{31} & \varepsilon_{32} & \varepsilon_{33} \end{bmatrix} \cdot \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix}$ .

Eg. For an anisotropic medium characterized by  $\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \varepsilon_0 \begin{bmatrix} 8 & 2 & 0 \\ 2 & 5 & 0 \\ 0 & 0 & 9 \end{bmatrix} \cdot \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix},$ 

find the value of the effective relative permittivity for (a)  $\vec{E} = \hat{z}E_0$ , (b)

$$\vec{E} = E_0(\hat{x} - 2\hat{y}), (c) \quad \vec{E} = E_0(2\hat{x} + \hat{y}).$$

(Sol.) (a) 
$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \varepsilon_0 \begin{bmatrix} 8 & 2 & 0 \\ 2 & 5 & 0 \\ 0 & 0 & 9 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} E_0 = \varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 9 \end{bmatrix} E_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} E_0, \quad \varepsilon_r = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 9\varepsilon_0 \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \varepsilon_0 = 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(b) 
$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \varepsilon_0 \begin{bmatrix} 8 & 2 & 0 \\ 2 & 5 & 0 \\ 0 & 0 & 9 \end{bmatrix} \cdot \begin{bmatrix} 1 \\ -2 \\ 0 \end{bmatrix} E_0 = \varepsilon_0 \begin{bmatrix} 4 \\ -8 \\ 0 \end{bmatrix} E_0 = 4\varepsilon_0 \begin{bmatrix} 1 \\ -2 \\ 0 \end{bmatrix} E_0, \quad \varepsilon_r = 4$$

(c) 
$$\begin{bmatrix} D_x \\ D_y \\ D_z \end{bmatrix} = \varepsilon_0 \begin{bmatrix} 8 & 2 & 0 \\ 2 & 5 & 0 \\ 0 & 0 & 9 \end{bmatrix} \cdot \begin{bmatrix} 2 \\ 1 \\ 0 \end{bmatrix} E_0 = \varepsilon_0 \begin{bmatrix} 18 \\ 9 \\ 0 \end{bmatrix} E_0 = 9\varepsilon_0 \begin{bmatrix} 2 \\ 1 \\ 0 \end{bmatrix} E_0, \quad \varepsilon_r = 9$$

### **Hall Effect:**

Current density:  $\vec{J} = \hat{y}J_0 = Nq\vec{v}$ 

If the material is a conductor or an n-type semiconductor the charge carrier are electrons: q < 0

*Hall field*: 
$$\vec{E}_h = -\vec{v} \times \vec{B} = -(\hat{y}v_0) \times (\hat{z}B_0) = -\hat{x}v_0B_0$$

*Hall voltage*: 
$$V_h = -\int_0^d E_h dx = v_0 B_0 d$$

Hall coefficient: 
$$C_h = \frac{E_x}{J_y B_z} = \frac{1}{Nq} < 0$$



*Hall field*: 
$$\vec{E}_h = \hat{x}v_0B_0$$

*Hall voltage*: 
$$V_h = -v_0 B_0 d$$

Hall coefficient: 
$$C_h > 0$$

#### 2-2 Boundary Conditions of Electromagnetic Fields

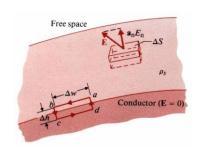
#### **Boundary conditions for electric fields:**

Eg. Show that  $E_t$ =0 on the conductor plane.

(Proof) : The E-field inside a conductor is zero,

$$\therefore \oint \vec{E} \cdot d \vec{l} = E_t \Delta W = 0 \Rightarrow E_t = 0$$

$$\oiint \vec{E} \cdot d \vec{S} = E_n \Delta S = \frac{\rho_s \Delta S}{\varepsilon} \Rightarrow E_n = \frac{\rho_s}{\varepsilon}$$



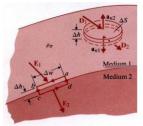
Eg. Show that  $E_{1t} = E_{2t}$  and  $\hat{a}_{n2} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_s$  on the interface between two

dielectric.

(Proof) 
$$\oint_{abcda} \vec{E} \cdot d \vec{l} = E_{1t} \Delta W - E_{2t} \Delta W = 0, E_{1t} = E_{2t}$$

$$\oiint_{abcda} \vec{D} \cdot d \vec{S} = \left( \vec{D_1} \cdot \vec{a_{n2}} + \vec{D_2} \cdot \vec{a_{n1}} \right) \Delta S = \vec{a_{n2}} \cdot (D_1 - D_2) \Delta S = \rho_s \Delta S$$

$$\vec{a_{n2}} \cdot \left( \vec{D_1} - \vec{D_2} \right) = \rho_s \text{ or } D_{1n} - D_{2n} = \rho_s$$

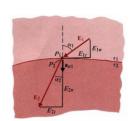


If  $\rho_s$ =0, then  $D_{1n}$ = $D_{2n}$  or  $\varepsilon_1 E_{1n}$ = $\varepsilon_2 E_{2n}$ 

Eg. Two dielectric media are separated by a charge free boundary. The electric field intensity in media 1 at the point  $P_1$  has a magnitude  $E_1$  and makes an angle  $\alpha_1$  with the normal. Determine the magnitude and direction of the electric field intensity at point  $P_2$  in medium 2. [交大電子所]

(Sol.) 
$$E_2 \sin \alpha_2 = E_1 \sin \alpha_1$$
,  $\varepsilon_2 E_2 \cos \alpha_2 = \varepsilon_1 E_1 \cos \alpha_1 \Rightarrow \frac{\tan \alpha_2}{\tan \alpha_1} = \frac{\varepsilon_2}{\varepsilon_1}$ 

$$\begin{split} E_2 &= \sqrt{E_{2t}^2 + E_{2n}^2} = \sqrt{\left(E_2 \sin \alpha_2\right)^2 + \left(E_2 \cos \alpha_2\right)^2} \\ &= \left[ \left(E_1 \sin \alpha_1\right)^2 + \left(\frac{\varepsilon_1}{\varepsilon_2} E_1 \cos \alpha_1\right)^2 \right]^{1/2} = E_1 \left[ \sin^2 \alpha_1 + \left(\frac{\varepsilon_1}{\varepsilon_2} \cos \alpha_1\right)^2 \right]^{1/2} \end{split}$$



Eg. Assume that z=0 plane separates two lossless dielectric regions with  $\varepsilon_{r1}=2$  and  $\varepsilon_{r2}=3$ . If  $\vec{E_1}$  in region 1 is  $\hat{x}2y-\hat{y}3x+\hat{z}(5+z)$ , find  $\vec{E_2}$  and  $\vec{D_2}$  at z=0 in region 2.

(Sol.) 
$$\vec{E_1} = \hat{x} 2y - \hat{y} 3x + \hat{z} 5$$
,  $\vec{E_{1t}}(z=0) = \vec{E_{2t}}(z=0) = \hat{x} 2y - \hat{y} 3x$ ,  
 $\vec{D_{1n}}(z=0) = \vec{D_{2n}}(z=0) \implies 2\vec{E_{1n}}(z=0) = 3\vec{E_{2n}}(z=0)$   
 $\vec{E_{2n}}(z=0) = \frac{2}{3}(\hat{z} 5) = \hat{z} \frac{10}{3}$ ,  $\vec{E_2}(z=0) = \hat{x} 2y - \hat{y} 3x + \hat{z} \frac{10}{3}$   
 $\vec{D_2}(z=0) = (\hat{x} 2y - \hat{y} 3x + \hat{z} \frac{10}{3}) 3\varepsilon_0$ 

Eg. A lucite sheet ( $\varepsilon_r$ =3.2) is introduced perpendicularly in a uniform electric field  $\vec{E_0} = \hat{x} E_0$  in free space. Determine  $\vec{E_i}$ ,  $\vec{D_i}$  and  $\vec{P_i}$  inside the lucite. [中央地球物理所]

(Sol.) 
$$\overrightarrow{D_i} = \overset{\wedge}{x} D_i = \overset{\wedge}{x} D_0 = \overset{\wedge}{x} \varepsilon_0 E_0$$

$$\overrightarrow{E_i} = \frac{1}{\varepsilon} \overset{\wedge}{D_i} = \frac{1}{\varepsilon_0 \varepsilon_r} \overset{\wedge}{D_i} = \overset{\wedge}{x} \frac{E_0}{3.2}$$

$$\overrightarrow{P_i} = \overset{\wedge}{D_i} - \varepsilon_0 \overset{\wedge}{E_i} = \overset{\wedge}{x} \left(1 - \frac{1}{3.2}\right) \varepsilon_0 E_0 = \overset{\wedge}{x} \frac{11}{16} \varepsilon_0 E_0 \quad (C/m)$$

Eg. Dielectric lenses can be used to collimate electromagnetic fields. The left surface of the lens is that of a circular cylinder, and right surface is a plane. If  $\vec{E}_1$  at point  $P(r_0,45^\circ,z)$  in region 1 is  $\hat{a_r} 5 - \hat{a_\phi} 3$ , what must be the dielectric constant of the lens in order that  $\vec{E}_3$  in region 3 is parallel to the x-axis?

(Sol.) Assume 
$$\vec{E_2} = \hat{a_r} E_{2r} + \hat{a_\phi} E_{2\phi}$$
,  $\therefore E_{1r} = E_{2r} = E_{\phi} \Rightarrow E_{2\phi} = -3$   
For  $\vec{E_3}$  //  $x - axis \Rightarrow \vec{E_2}$  //  $x - axis \Rightarrow E_{2\phi} = -E_{2r} \Rightarrow E_{2r} = 3$   
 $\hat{a_n} \cdot \vec{D_1} = \hat{a_n} \cdot \vec{D_2} \Rightarrow \varepsilon_1 E_{r1} = \varepsilon_2 E_{r2}$ ,  $\varepsilon_0 5 = \varepsilon_0 \varepsilon_{r2} 3 \Rightarrow \varepsilon_{r2} = \frac{5}{3}$ 

# Eg. A positive point charge Q is at the center of a spherical dielectric shell of an inner radius $R_i$ and an outer radius $R_o$ . The dielectric constant of the shell is $\varepsilon_r$ .

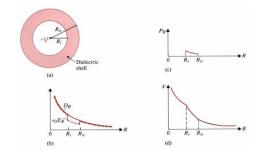
Determine  $\overset{\rightarrow}{E}$ , V,  $\overset{\rightarrow}{D}$ , and  $\overset{\rightarrow}{P}$  as functions of the radial distance R. [高考]

(Sol.) 
$$\overrightarrow{P} = \overrightarrow{D} - \varepsilon_0 \overrightarrow{E} = \varepsilon_0 (\varepsilon_r - 1) \overrightarrow{E}$$

 $R>R_0$ :

$$\vec{E} = \hat{a}_R \frac{Q}{4\pi\varepsilon_0 R^2}, \ V = \frac{Q}{4\pi\varepsilon_0 R}$$

$$\vec{D} = \hat{a}_R \frac{Q}{4\pi R^2} \quad \text{and} \quad \vec{P} = 0$$



 $R_i < R < R_o$ :

$$\vec{E} = \hat{a}_R \frac{Q}{4\pi\varepsilon_0 \varepsilon_r R^2} = \hat{a}_R \frac{Q}{4\pi \mathcal{R}^2} , \quad \vec{D} = \hat{a}_R \frac{Q}{4\pi R^2} , \quad \vec{P} = \hat{a}_R \bigg( 1 - \frac{1}{\varepsilon_r} \bigg) \frac{Q}{4\pi R^2}$$

$$V = -\int_{\infty}^{R_o} \frac{Q}{4\pi\varepsilon_0 R^2} dR - \int_{R_o}^{R} \frac{Q}{4\pi\varepsilon_0 \varepsilon_r R^2} dR = \frac{Q}{4\pi\varepsilon_0} \left[ \left( 1 - \frac{1}{\varepsilon_r} \right) \frac{1}{R_o} + \frac{1}{\varepsilon_r R} \right]$$

$$R < R_i$$
:  $\vec{E} = \hat{a}_R \frac{Q}{4\pi\epsilon_0 R^2}$ ,  $\vec{D} = \hat{a}_R \frac{Q}{4\pi R^2}$ ,  $\vec{P} = 0$ ,

$$V = V \bigg|_{R = R_i} - \int_{R_i}^{R} \frac{Q}{4\pi\varepsilon_0 R^2} dR = \frac{Q}{4\pi\varepsilon_0} \left[ \left( 1 - \frac{1}{\varepsilon_r} \right) \frac{1}{R_o} - \left( 1 - \frac{1}{\varepsilon_r} \right) \frac{1}{R_i} + \frac{1}{R} \right]$$

## **Boundary conditions for magnetic fields:**

Eg. Show that  $\mu_1 H_{1n} = \mu_2 H_{2n}$  and  $\hat{a}_{n2} \times (\overrightarrow{H}_1 - \overrightarrow{H}_2) = \overrightarrow{J}$ .

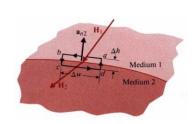
(Proof) 
$$\iint \vec{B} \cdot d\vec{S} = 0 \Rightarrow B_{1n} \Delta S - B_{2n} \Delta S = 0, B_{1n} = B_{2n}$$

$$\Rightarrow \mu_1 H_{1n} = \mu_2 H_{2n}$$

$$\oint \overrightarrow{H} \cdot d\overrightarrow{l} = I \Rightarrow \oint \overrightarrow{H} \cdot d\overrightarrow{l} = H_1 \cdot \Delta w + H_2 \cdot (-\Delta w) = J_{sw} \Delta w$$

$$\Rightarrow H_{1t} - H_{2t} = J_{sw} \Rightarrow \hat{a}_{n2} \times (\overrightarrow{H}_1 - \overrightarrow{H}_2) = \overrightarrow{J}$$

If 
$$J=0$$
, then  $H_{1t}=H_{2t}$ 



Eg. Two magnetic media with permeabilities  $\mu_1$  and  $\mu_2$  have a common boundary. The magnetic field intensity in medium 1 at the point  $P_1$  has a magnitude  $H_1$  and makes an angle  $\alpha_1$  with the normal. Determine the magnitude and the direction of the magnetic field intensity at point  $P_2$  in medium 2.

(Sol.) 
$$\begin{cases} \mu_2 H_2 \cos \alpha_2 = \mu_1 H_1 \cos \alpha_1 \\ H_2 \sin \alpha_2 = H_1 \sin \alpha_1 \end{cases} \Rightarrow \frac{\tan \alpha_2}{\tan \alpha_1} = \frac{\mu_2}{\mu_1}$$

$$\Rightarrow \alpha_2 = \tan^{-1}(\frac{\mu_2}{\mu_1}\tan\alpha_1)$$

$$H_2 = \sqrt{H_{2t}^2 + H_{2n}^2} = \sqrt{(H_2 \sin \alpha_2)^2 + (H_2 \cos \alpha_2)^2} = H_1 \left[ \sin^2 \alpha_1 + (\frac{\mu_1}{\mu_2} \cos \alpha_1)^2 \right]^{\frac{1}{2}}$$

Eg. Consider a plane boundary (y=0) between air (region 1,  $\mu_{r1}=1$ ) and iron (region 2,  $\mu_{r2}=5000$ ). (a) Assuming  $\vec{B}_1 = 0.5\hat{x} - 10\hat{y}$  (mT), find  $\vec{B}_2$  and the angle

that  $\overline{B}_2$  makes with the interface. (b) Assuming  $\vec{B}_2 = 10\hat{x} + 0.5\hat{y}$  (mT), find  $\overline{B}_1$  and the angle that  $\vec{B}_1$  makes with the normal to the interface. (Sol.)

(a) 
$$\vec{B}_1 = 0.5\hat{x} - 10\hat{y}$$
,  $\vec{B}_2 = B_{2x}\hat{x} + B_{2y}\hat{y}$ ,  $H_{2x} = \frac{B_{2x}}{5000 \,\mu_o} = H_{1x} = \frac{0.5}{\mu_o} \Rightarrow B_{2x} = 2500$ 

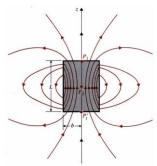
$$B_{2y} = B_{1y} = -10 \implies \vec{B}_2 = 2500 \,\hat{x} - 10 \,\hat{y}, \quad \tan \alpha_2 = \frac{\mu_2}{\mu_1} \tan \alpha_1 = 500 \frac{B_{1x}}{B_{1y}} = 25$$

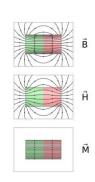
(b) 
$$\vec{B}_2 = 10\hat{x} + 0.5\hat{y}$$
,  $\vec{B}_1 = B_{1x}\hat{x} + B_{1y}\hat{y}$ ,  $H_{1x} = \frac{B_{1x}}{\mu_1} = H_{2x} = \frac{B_{2x}}{\mu_2}$ 

$$\Rightarrow B_{1x} = \frac{1}{\mu_{BE}} B_{2x} = \frac{10}{5000} = 0.002, \quad B_{1y} = B_{2y} = 0.5, \quad \vec{B}_1 = 0.002 \,\hat{x} + 0.5 \,\hat{y},$$

$$\tan \alpha_1 = \frac{B_{1x}}{B_{1x}} = \frac{0.002}{0.5} = 0.004$$

Magnetic flux lines round a cylindrical bar magnet:





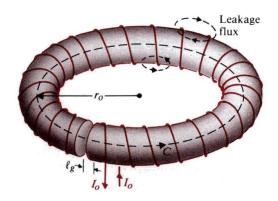
Eg. Assume that N turns of wire are wound around a toroidal core of a ferromagnetic material with permeability  $\mu$ . The core has a mean radius  $r_0$ , a circular cross section of radius a ( $a \ll r_0$ ), and a narrow air gap of length  $l_g$ , as shown in Figure. A steady current  $I_0$  flows in the wire. Determine (a) the magnetic flux density  $B_f$  in the ferromagnetic core; (b) the magnetic field intensity  $H_f$  in the core; and, (c) the magnetic field intensity  $H_g$  in the gap. [台大電研]

(Sol.)

$$\oint_{C} \vec{H} \cdot d\vec{l} = NI_{o}, \quad \vec{B}_{f} = \vec{B}_{g} = \hat{a}_{\phi} B_{f}, \quad \frac{B_{f}}{\mu} (2\pi r_{o} - l_{g}) + \frac{B_{f}}{\mu_{o}} l_{g} = NI_{o}$$

$$B_{f} = \frac{\mu_{o} \, \mu N I_{o}}{\mu_{o} \left(2\pi r_{o} - l_{g}\right) + \mu l_{g}} \Rightarrow \overset{\longrightarrow}{H}_{f} = \hat{a}_{\phi} \, \frac{\mu_{o} \, N I_{o}}{\mu_{o} \left(2\pi r_{o} - l_{g}\right) + \mu l_{g}}$$

$$\overrightarrow{H}_{g} = \hat{a}_{\phi} \frac{\mu NI_{o}}{\mu_{o} (2\pi r_{o} - l_{g}) + \mu l_{g}}$$



Boundary Conditions between a Dielectric (Medium 1) and a Perfect Conductor (Medium 2) (Time-Varying Case)

On the Side of Medium 1	On the Side of Medium 2
$E_{1t} = 0$	$E_{2t} = 0$
$\mathbf{a}_{n2} \times \mathbf{H}_1 = \mathbf{J}_s$	$H_{2t} = 0$
$\mathbf{a}_{n2} \cdot \mathbf{D}_1 = \rho_s$	$D_{2n}=0$
$B_{1n} = 0$	$B_{2n} = 0$

# Boundary Conditions between Two Lossless Media

$$E_{1t} = E_{2t} \to \frac{D_{1t}}{D_{2t}} = \frac{\epsilon_1}{\epsilon_2}$$

$$H_{1t} = H_{2t} \to \frac{B_{1t}}{B_{2t}} = \frac{\mu_1}{\mu_2}$$

$$D_{1n} = D_{2n} \to \epsilon_1 E_{1n} = \epsilon_2 E_{2n}$$

$$B_{1n} = B_{2n} \to \mu_1 H_{1n} = \mu_2 H_{2n}$$

#### 2-3 Steady-state Currents

**Differential current:** 
$$\Delta I = \frac{\Delta Q}{\Delta t} = \frac{Nq\vec{v} \cdot \hat{a}_n \Delta s \Delta t}{\Delta t} = Nq\vec{v} \cdot \Delta \vec{s}$$

**Current density:** 
$$\vec{J} = Nq\vec{v} = \rho\vec{v}$$
  $(A/m^2)$ ,  $I = \iint_{S} \vec{J} \cdot d\vec{S}$  (A)



Let 
$$\vec{v} = \mu \vec{E}$$
,  $\vec{J} = \rho \vec{v} = -\mu \rho \vec{E} = \sigma \vec{E}$ 

$$\mu$$
: mobility  $\sigma$ : conductivity

$$\sigma = -\rho_e u_e + \rho_h u_h$$
electrons holes

Eg. An  $emf\ V$  is applied across a parallel-plate capacitor of area S. The space between the conducting plates is filled with two different lossy dielectrics of

thicknesses  $d_1$  and  $d_2$ , permittivities  $\varepsilon_1$  and  $\varepsilon_2$ , and conductivities  $\sigma_1$  and  $\sigma_2$ , respectively. Determine (a) the current density between the plates, (b) the electric field intensities in both dielectrics. [高考]



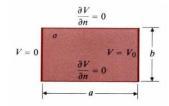
(Sol.)

$$V = (R_1 + R_2)I = \left(\frac{d_1}{\sigma_1 S} + \frac{d_2}{\sigma_2 S}\right)I$$

$$J = \frac{I}{S} = \frac{V}{(d_1/\sigma_1) + (d_2/\sigma_2)} = \frac{\sigma_1 \sigma_2 V}{\sigma_2 d_1 + \sigma_1 d_2}$$

$$V = E_1 d_1 + E_2 d_2, \quad J = \sigma_1 E_1 = \sigma_2 E_2, \quad E_1 = \frac{\sigma_2 V}{\sigma_2 d_1 + \sigma_1 d_2}, \quad E_2 = \frac{\sigma_1 V}{\sigma_2 d_1 + \sigma_1 d_2}$$

Eg. Assume a rectangular conducting sheet of conductivity  $\sigma$ , width a, and height b. A potential difference is applied to the side edges. Find (a) the potential distribution, (b) the current density everywhere within the sheet. [台科大電子所]



(Sol.)

(a) 
$$V(x)=Cx$$
,  $V(a)=Ca=V_0 \Rightarrow V(x)=\frac{V_o}{a}x$ 

(b) 
$$\vec{E} = -\nabla V(x) = -\hat{x}\frac{V_o}{a} \Rightarrow \vec{J} = \sigma \vec{E} = -\hat{x}\frac{\sigma V_o}{a}$$

Equation of continuity: 
$$I = \iint_{s} \vec{J} \cdot d\vec{S} = -\frac{dQ}{dt} = -\frac{d}{dt} \iiint_{v'} \rho dv = \iiint \nabla \cdot \vec{J} dv \Rightarrow \nabla \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$
  
If  $\vec{J} = \sigma \vec{E}$ ,  $\sigma \nabla \cdot \vec{E} + \frac{\partial p}{\partial t} = \sigma \frac{\rho}{s} + \frac{\partial \rho}{\partial t} = 0$ ,  $\rho = \rho_0 e^{-\frac{\sigma}{s}t}$ 

#### **Boundary conditions for current densities:**

$$\begin{cases} \nabla \cdot \vec{J} = 0 \Rightarrow \\ \nabla \times \left(\frac{\vec{J}}{\sigma}\right) = 0 \Rightarrow \begin{cases} J_{1n} = J_{2n} \\ J_{1t} = \frac{\sigma_1}{\sigma_2} \end{cases} \end{cases}$$

Governing Equations for Steady Current Density			
Differential Form Integral Form			
$\nabla \cdot \vec{J} = 0$	$\oint_{s} \vec{J} \cdot d\vec{s} = 0$		
$\nabla \times \left(\frac{\vec{J}}{\sigma}\right) = 0$	$\oint_c \frac{1}{\sigma} \vec{J} \cdot d\vec{\ell} = 0$		

Eg. Two conducting media with conductivities  $\sigma_1$  and  $\sigma_2$  are separated by an interface. The steady current density in medium 1 at point  $P_1$  has a magnitude  $J_1$  and makes an angle  $\alpha_1$  with the normal. Determine the magnitude and direction of the current density at point  $P_2$  in Medium 2. [台大電研]

(Sol.)

$$J_1 \cos \alpha_1 = J_2 \cos \alpha_2, \ \ \sigma_2 J_1 \sin \alpha_1 = \sigma_1 J_2 \sin \alpha_2 \Rightarrow \frac{\tan \alpha_2}{\tan \alpha_1} = \frac{\sigma_2}{\sigma_1}$$

$$\boldsymbol{J}_{2} = \sqrt{\boldsymbol{J}_{2t}^{2} + \boldsymbol{J}_{2n}^{2}} = \sqrt{(\boldsymbol{J}_{2} \sin \alpha_{2})^{2} + (\boldsymbol{J}_{2} \cos \alpha_{2})^{2}} = \left[ \left( \frac{\sigma_{2}}{\sigma_{1}} J_{1} \sin \alpha_{1} \right)^{2} + (J_{1} \cos \alpha_{1})^{2} \right]^{1/2}$$

$$\begin{cases} J_{1n} = J_{2n} \Rightarrow \sigma_1 E_{1n} = \sigma_2 E_{2n} \\ D_{1n} - D_{2n} = \rho_s \Rightarrow \varepsilon_1 E_{1n} - \varepsilon_2 E_{2n} = \rho_s \end{cases} \Rightarrow \rho_s = \left(\varepsilon_1 \frac{\sigma_2}{\sigma_1} - \varepsilon_2\right) E_{2n} = \left(\varepsilon_1 - \varepsilon_2 \frac{\sigma_1}{\sigma_2}\right) E_{1n}. \text{ If }$$

$$\sigma_2 >> \sigma_1 \Rightarrow \rho_s = \varepsilon_1 E_{1n} = D_{1n}.$$

#### 2-4 Maxwell's Equations and Plane EM Waves

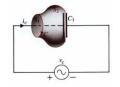
#### Maxwell's Equations

Differential Form	Integral Form	Significance		
$\mathbf{\nabla} \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$	$\oint_C \mathbf{E} \cdot d\boldsymbol{\ell} = -\frac{d\boldsymbol{\Phi}}{dt}$	Faraday's law		
$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$	$\oint_C \mathbf{H} \cdot d\boldsymbol{\ell} = I + \int_S \frac{\partial \mathbf{D}}{\partial t} \cdot d\mathbf{s}.$	Ampère's circuital law		
$\nabla \cdot \mathbf{D} = \rho$	$\oint_{S} \mathbf{D} \cdot d\mathbf{s} = Q$	Gauss's law		
$\mathbf{\nabla \cdot B} = 0$	$\oint_{\mathbf{S}} \mathbf{B} \cdot d\mathbf{s} = 0$	No isolated magnetic charge		

**Note:**  $\frac{\partial \bar{D}}{\partial t}$  is equivalent to a current density, called the displacement current density.

# Eg. A voltage source $V_0\sin(\omega t)$ , is connected across a parallel-plate capacitor C. Find the displacement current in the capacitor.

(Sol.) 
$$i_C = C \frac{dv_C}{dt} = CV_0 \omega \cos \omega t = \varepsilon \frac{A}{d} V_0 \omega \cos \omega t$$
  
 $\vec{D} = \varepsilon \vec{E} \Rightarrow D = \varepsilon \frac{V_0}{d} \sin \omega t$ 



$$i_D = \iint_A \frac{\partial \vec{D}}{\partial t} \cdot d\vec{S} = \varepsilon \frac{A}{d} V_0 \omega \cos \omega t = i_C$$

**Lorentz condition:**  $\nabla \cdot \vec{A} + \mu \varepsilon \frac{\partial V}{\partial t} = 0$ 

$$\nabla \times \vec{B} = \mu \vec{J} + \mu \frac{\partial \vec{D}}{\partial t} = \nabla \times \nabla \times \vec{A} = \mu \vec{J} + \mu \varepsilon \frac{\partial}{\partial t} (-\nabla V - \frac{\partial \vec{A}}{\partial t}) = \nabla (\nabla \cdot \vec{A}) - \nabla^2 \vec{A} = \mu \vec{J} - \nabla (\mu \varepsilon \frac{\partial V}{\partial t}) - \mu \varepsilon \frac{\partial^2 \vec{A}}{\partial t^2}$$

$$\Rightarrow \nabla^2 \vec{A} - \mu \varepsilon \frac{\partial^2 \vec{A}}{\partial t^2} = -\mu \vec{J} + \nabla (\nabla \cdot \vec{A} + \mu \varepsilon \frac{\partial V}{\partial t})$$

If Lorentz Condition holds, we have  $\nabla^2 \vec{A} - \mu \varepsilon \frac{\partial^2 \vec{A}}{\partial t^2} = -\mu \vec{J}$ 

$$\vec{\nabla} \cdot \vec{D} = \rho = \nabla \cdot \varepsilon \vec{E} = \rho = \nabla \cdot \varepsilon (-\nabla V - \frac{\partial \vec{A}}{\partial t}) \Rightarrow \nabla^2 V + \frac{\partial}{\partial t} (\nabla \cdot \vec{A}) = \nabla^2 V + \frac{\partial}{\partial t} (-\mu \varepsilon \frac{\partial V}{\partial t}) = -\frac{\rho}{\varepsilon}$$

$$\therefore \nabla^2 V - \mu \varepsilon \frac{\partial^2 V}{\partial t^2} = -\frac{\rho}{\varepsilon}$$

#### **Effective permittivity:**

$$\nabla \times \vec{H} = \vec{J} + \varepsilon \frac{\partial \vec{E}}{\partial t} = \sigma \vec{E} + j\omega \varepsilon \vec{E} = j\omega(\varepsilon + \frac{\sigma}{j\omega})\vec{E} = j\omega\varepsilon_C \vec{E}$$

$$\Rightarrow \varepsilon_C = \varepsilon - j \frac{\sigma}{\omega} = \varepsilon' - j \varepsilon'' \Rightarrow \sigma = \omega \varepsilon''$$
. Similarly,  $\mu = \mu' - j \mu''$ 

**Loss tangent:** 
$$\tan \delta_C = \frac{\varepsilon''}{\varepsilon'} = \frac{\sigma}{\omega \varepsilon}$$

Eg. A sinusoidal electric intensity of amplitude 250V/m and frequency 1GHz exists in a lossy dielectric medium that has a relative permittivity of 2.5 and loss tangent of 0.001. Find the average power dissipated in the medium per cubic meter.

(Sol.)

$$\tan \delta_{\varepsilon} = 0.001 = \frac{\sigma}{\omega \varepsilon_{0} \varepsilon_{r}},$$

$$\sigma = 0.001(2\pi 10^{9})(\frac{10^{-9}}{36\pi})(2.5) = 1.39 \times 10^{-4} (S/m)$$

$$p = \frac{1}{2}JE = \frac{1}{2}\sigma E^{2} = \frac{1}{2} \times (1.39 \times 10^{-4}) \times 250^{2} = 4.34(W/m^{3})$$

#### Maxwell's Equations in the source-free regions:

$$\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t}, \quad \nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t}, \quad \nabla \cdot \vec{E} = 0, \quad \nabla \cdot \vec{H} = 0$$

**Phasor representations:** Eg.  $\hat{x}Ae^{-j(\beta x+\theta)}$ ,  $(\hat{x}\frac{3}{5}+\hat{y}\frac{4}{5})e^{-j(\beta x+\theta)}$ , etc.

**Instantaneous representations:** Eg.  $\hat{x}A\cos(\omega t - \beta z + \theta) = \text{Re}[\hat{x}Ae^{-j(\beta z + \theta)} \cdot e^{j\omega t}]$ , etc.

In case  $\vec{E}$  and  $\vec{H}$  are proportional to  $e^{j\omega t}$ , we have  $\nabla \times \vec{E} = -\mu \frac{\partial H}{\partial t} = -j\omega \mu \vec{H}$ ,

$$\nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t} = j \omega \varepsilon \vec{E}$$
, and  $k_x^2 + k_y^2 + k_z^2 = k_x^2 + k_y^2 + \beta^2 = k^2 = \omega^2 \mu \varepsilon$ .

Eg. Given that  $\vec{H} = \hat{y}2\cos(15\pi x)\sin(6\pi 10^9 t - \beta z)$  in air, find  $\vec{E}$  and  $\beta$ .

(Sol.) *Phasor*:  $\vec{H} = \hat{y} 2\cos(15\pi x)e^{-j\beta z}$ ,  $(15\pi)^2 + \beta^2 = \omega^2 \mu_0 \varepsilon_0 = 400\pi^2 \Rightarrow \beta = 13.2\pi$ 

$$\vec{E} = \frac{1}{j\omega\varepsilon_0} \nabla \times \vec{H} = [\hat{x}158\pi\cos(15\pi x) + \hat{z}j180\pi\sin(15\pi x)]e^{-j\beta z}$$

$$\vec{E}(x,z,t) = \text{Re}[\vec{E}(x,z)e^{j\omega t}]$$

**Eg.** Given that  $\vec{E} = \hat{y}0.1\cos(10\pi x)\sin(6\pi 10^9 t - \beta z)$  in air, find  $\vec{H}$  and  $\beta$ .

(Sol.) Phasor:  $\vec{E} = \hat{y}0.1\cos(10\pi x)e^{-j\beta z}$ ,  $(10\pi)^2 + \beta^2 = \omega^2 \mu_0 \varepsilon_0 = 400\pi^2 \Rightarrow \beta = 10\sqrt{3}\pi$ 

$$\vec{H} = -\frac{1}{j\omega\mu_0} \nabla \times \vec{E} = \frac{j}{\omega\mu_0} [\hat{x}0.1\beta\cos(10\pi x) + \hat{z}0.1(10\pi)\cos(10\pi x)]e^{-j\beta x}$$

$$\vec{H}(x,z,t) = \text{Re}[\vec{H}(x,z)e^{j\omega t}]$$

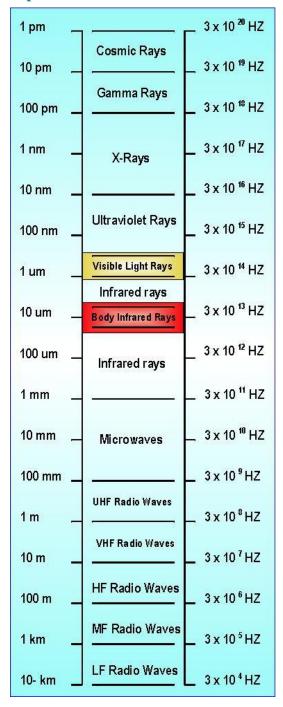
#### Plane EM waves excited by a current sheet:

Given  $\vec{J}(t) = -\hat{x}J(t)$  at z=0, the field components of the EM plane wave excited by the current density are  $\vec{E}(z,t) = \hat{x}\frac{\eta}{2}J(t\mp\frac{z}{v_p})$  and  $\vec{H}(z,t) = \pm\hat{y}\frac{1}{2}J(t\mp\frac{z}{v_p})$ ,

respectively. If it is a sinusoidal EM plane wave,  $\vec{J}(t) = -\hat{x}J_0 \cos(\omega t)$  at z=0.

We have 
$$\vec{E}(z,t) = \hat{x} \frac{\eta J_0}{2} \cos(\omega t \mp kz)$$
,  $\vec{H}(z,t) = \pm \hat{y} \frac{J_0}{2} \cos(\omega t \mp kz)$ .

## **Electromagnetic wave spectrum:**



#### 2-5 Plane EM waves in a simple, nonconducting and source-free region

In a simple, nonconducting and source-free region:

$$\nabla \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \,, \ \, \nabla \times \vec{H} = \varepsilon \frac{\partial \vec{E}}{\partial t} \,, \ \, \nabla \cdot \vec{E} = 0 \,, \ \, \nabla \cdot \vec{H} = 0$$

$$\nabla \times \nabla \times E = -\mu \frac{\partial}{\partial t} (\nabla \times \vec{H}) = -\mu \varepsilon \frac{\partial^2 E}{\partial t^2} = \nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = -\nabla^2 \vec{E} \implies \nabla^2 \vec{E} - \mu \varepsilon \frac{\partial^2 \vec{E}}{\partial t^2} = 0.$$

**Velocity** of the plane EM wave:  $v = \frac{1}{\sqrt{\mu \varepsilon}}$ 

In vacuum,  $\mu_0 = 4\pi \times 10^{-7}$ ,  $\varepsilon_0 = \frac{1}{36\pi} \times 10^{-9} \Rightarrow c = \frac{1}{\sqrt{\mu_0 \varepsilon_0}} \approx 3 \times 10^8 (m/s)$ .

Wave number: 
$$k=\omega/v=\omega\sqrt{\mu\varepsilon} = \frac{2\pi}{v/f} = \frac{2\pi}{\lambda}$$

Assume  $\vec{E} \propto e^{j\omega t} \Rightarrow \nabla^2 \vec{E} + k^2 \vec{E} = 0$  (drop  $e^{j\omega t}$  factor)

Suppose 
$$\vec{E} = \vec{E}(z) \Rightarrow \frac{d^2 \vec{E}(z)}{dz^2} + k^2 \vec{E} = 0 \Rightarrow \vec{E}(z) = E_0^+ e^{-jkz} + E_0^- e^{jkz}$$

**Traveling wave in +z-direction:** 

$$E_0^+(z,t) = \text{Re}[E_0^+ e^{-jkz} \cdot e^{j\omega t}] = E_0^+ \cos(\omega t - kz)$$

Let  $\omega t$ -kz=constant  $\Rightarrow$  Phase velocity:  $v_p = \frac{dz}{dt} = \frac{\omega}{k}$ 

If 
$$\vec{E} = \hat{x}E_x^+(z), \nabla \times \vec{E} = -j\omega\mu(\hat{x}H_x^+ + \hat{y}H_y^+ + \hat{z}H_z^+)$$

$$\Rightarrow H_x^+ = H_z^+ = 0, \ H_y^+(z) = -\frac{1}{j\omega\mu} \cdot (-jk)E_x^+(z) = \frac{1}{\eta}E_x^+(z), \text{ where } \eta = \frac{\omega\mu}{k} = \sqrt{\frac{\mu}{\varepsilon}},$$

and  $\eta_0=120\pi \approx 377\Omega$  in free space.

TEM waves (Transverse electromagnetic waves):  $\vec{E}$  and  $\vec{H} \perp$  direction of propagation  $(\hat{a}_n)$ 

$$\vec{E}(\vec{R}) = \vec{E}(x, y, z) = \vec{E}_0 e^{-jk_x x - jk_y y - jk_z z} = \vec{E}_0 e^{-j\bar{k}\cdot\bar{R}} = \vec{E}_0 e^{-jk\hat{a}_n\cdot\bar{R}} , \text{ where } \vec{R} = \hat{x}x + \hat{y}y + \hat{z}z ,$$

$$\vec{k} = \hat{a}_n k$$
, and  $k_x^2 + k_y^2 + k_z^2 = \omega^2 \mu \varepsilon$ 

$$\hat{a}_n \cdot \vec{E}_0 = 0 \Rightarrow \vec{E}_0 \perp \hat{a}_n \quad \text{(TE)}. \text{ Similarly, } \nabla \cdot \vec{H} = 0 \Rightarrow \vec{H}_0 \perp \hat{a}_n \quad \text{(TM)}$$

#### Relation between E-field and H-field of the plane EM wave:

$$\vec{E}(\vec{R}) = \frac{1}{j\omega\varepsilon} \nabla \times \vec{H}(\vec{R}) = \frac{1}{j\omega\varepsilon} (-jk) \hat{a}_n \times \vec{H}(\vec{R}) \Rightarrow \vec{E}(\vec{R}) = -\eta \hat{a}_n \times \vec{H}(\vec{R}), \text{ where } \eta = \frac{\omega\mu}{k} = \sqrt{\frac{\mu}{\varepsilon}}$$

$$\vec{H}(\vec{R}) = -\frac{1}{j\omega\mu} \nabla \times \vec{E}(\vec{R}) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(\vec{R}) \Rightarrow \vec{H}(\vec{R}) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(R) \Rightarrow \vec{H} \perp \hat{a}_n$$

Eg. The instantaneous expression for the magnetic field intensity of a uniform plane wave propagating in the +y direction in air is given by  $\bar{H} = \hat{z}4 \times 10^{-6} \cos(10^7 \pi t - k_0 y + \frac{\pi}{4})$  A/m. (a) Determine  $k_0$  and the location where  $H_z$  vanishes at t=3ms. (b) Write the instantaneous expression for  $\bar{E}$ .

(Sol.) 
$$\omega = 10^7 \pi \Rightarrow k_0 = \frac{\omega}{c} = \frac{10^7 \pi}{3 \times 10^8} = \frac{\pi}{30}, \ \hat{a}_n = \hat{y}$$

(a) 
$$\cos[(2n+1)\frac{\pi}{2}] = 0 \Rightarrow 10^7 \pi \times 3 \times 10^{-3} - \frac{\pi}{30}y + \frac{\pi}{4} = \frac{2n+1}{2}\pi \Rightarrow y = 30(3 \times 10^4 - \frac{1}{4} - n)$$

(b) 
$$\vec{E}(z,t) = -\eta_0 \hat{a}_n \times \vec{H}(z,t)$$
,  $\vec{E}(z,t) = -\hat{x}480\pi 10^{-6} \cos(10^7 \pi t - \frac{\pi}{30} y + \frac{\pi}{4})$ 

Eg. A 100MHz uniform plane wave  $\vec{E} = \hat{x}E_x$  propagates in the +z direction.

Suppose  $\varepsilon_r$ =4,  $\mu_r$ =1,  $\sigma$ =0, and it has a maximum value of  $10^{-4}V/m$  at t =0 and z=0.125m. (a) Write the instantaneous expressions for  $\vec{E}$  and  $\vec{H}$ . (b) Determine the location where  $\vec{E}$  is a positive maximum when t=10<sup>-8</sup>sec.

(Sol.) 
$$k = \omega \sqrt{\mu_0 \mu_r \varepsilon_0 \varepsilon_r} = \frac{4\pi}{3}, \hat{a}_n = \hat{z}, \eta = \sqrt{\frac{\mu_0 \mu_r}{\varepsilon_0 \varepsilon_r}} = 60\pi$$

(a)  $\vec{E}(z,t) = \hat{x}E_x = \hat{x}10^{-4}\cos(2\pi \times 10^8 t - kz + \theta)$  has the maximum in case of

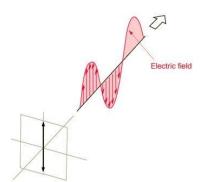
$$2\pi \times 10^8 t - kz + \theta = 0 \Rightarrow \theta = \frac{\pi}{6} \Rightarrow \vec{E}(z,t) = \hat{x}10^{-4} \cos(2\pi 10^8 t - \frac{4\pi}{3} z + \frac{\pi}{6}),$$

$$\vec{H}(z,t) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(z,t) = \hat{y} \frac{10^{-4}}{60\pi} \cos(2\pi 10^8 t - \frac{4\pi}{3} z + \frac{\pi}{6})$$

(b) 
$$\cos(2n\pi) = 1$$
,  $2\pi 10^8 (10^{-8}) - \frac{4\pi}{3} z_{\text{max}} + \frac{\pi}{6} = 2n\pi \Rightarrow z_{\text{max}} = \frac{13}{8} \pm \frac{3n}{2}$ 

Polarization of the EM wave: The direction of electric field of the EM wave.

In the following text, we assume all EM waves to be z-propagated if we do not specify them.



<u>Linear polarizations</u> in the x and the y-direction,

**respectively:** 
$$\vec{E} = \hat{x}E_x e^{-j(kz+\theta)}$$
,  $\vec{E} = \hat{y}E_y e^{-j(kz+\theta)}$ 

Linear polarization in general case:

$$\vec{E} = \hat{x}E_x e^{-j(kz+\theta)} + \hat{y}E_y e^{-j(kz+\theta)}$$
, where  $E_x$  and  $E_y$  are in

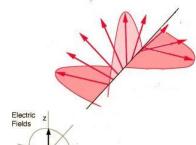
phase (we can assume the both to be real).

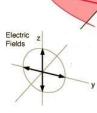
<u>circular</u> polarization: Right-hand

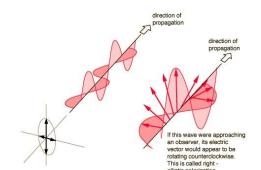
$$\vec{E} = \hat{x}E_0e^{-j(kz+\theta)} - \hat{y}jE_0e^{-j(kz+\theta)}$$

circular Left-hand polarization:

$$\vec{E} = \hat{x}E_0e^{-j(kz+\theta)} + \hat{y}jE_0e^{-j(kz+\theta)}$$







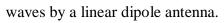
Right-hand elliptical polarization:

$$\vec{E} = \hat{x} E_{10} e^{-j(kz+\theta)} - \hat{y} j E_{20} e^{-j(kz+\theta)} \ \ (E_{10} \neq E_{20})$$

Left-hand elliptical polarization:

$$\vec{E} = \hat{x} E_{10} e^{-j(kz+\theta)} + \hat{y} j E_{20} e^{-j(kz+\theta)} \ \ (E_{10} \neq E_{20})$$

We can receive/transmit linearly-polarized EM









Circular reflector antenna.









Instantaneous Expression for  $\vec{E}$  of right-hand elliptical-polarization (drop phase factor  $e^{-j\theta}$ ):

$$\vec{E}(z,t) = \text{Re}\left\{ [\hat{x}E_{10}e^{-jkz} - \hat{y}jE_{20}e^{-jkz}]e^{j\omega t} \right\} = \hat{x}E_{10}\cos(\omega t - kz) + \hat{y}E_{20}\sin(\omega t - kz)$$
$$= \hat{x}E_{1}(z,t) + \hat{y}E_{2}(z,t)$$

$$\Rightarrow \cos(\omega t) = \frac{E_1(0,t)}{E_{10}}, \quad \sin(\omega t) = \frac{E_2(0,t)}{E_{20}} \Rightarrow \left[\frac{E_1(0,t)}{E_{10}}\right]^2 + \left[\frac{E_2(0,t)}{E_{20}}\right]^2 = 1, \quad \omega t = \tan^{-1}\frac{E_2(0,t)}{E_1(0,t)}$$

1.  $\hat{x}E_x = \frac{1}{2}(\hat{x}E_x - \hat{y}jE_y) + \frac{1}{2}(\hat{x}E_x + \hat{y}jE_y)$ : A linearly polarized plane wave can be

resolved into a right -hand and left-hand elliptically- or circularly-polarized waves.

2. 
$$\hat{x}E_0 - \hat{y}jE_0 = (\hat{x}\frac{E_0 + E_1}{2} - \hat{y}j\frac{E_1 - E_0}{2}) + (\hat{x}\frac{E_0 - E_1}{2} + \hat{y}j\frac{E_0 + E_1}{2})$$
:

A circularly–polarized plane wave can be resolved into two opposite elliptically–polarized waves.

3. 
$$\hat{x}E_1 - \hat{y}jE_2 = (\hat{x}\frac{E_{.1} + E_2}{2} - \hat{y}j\frac{E_1 + E_2}{2}) + (\hat{x}\frac{E_1 - E_2}{2} + \hat{y}j\frac{E_1 - E_2}{2})$$
:

An elliptically-polarized plane wave can be resolved into two opposite circularly-polarized waves.

Eg. The  $\vec{E}$  field of a uniform plane wave propagating in a dielectric medium is given by  $E(t,z) = \hat{x}2\cos(10^8t - \frac{z}{\sqrt{3}}) - \hat{y}\sin(10^8t - \frac{z}{\sqrt{3}})$  V/m. (a) Determine the

frequency and wavelength of the wave. (b) What is the dielectric constant of the medium? (c) Describe the polarization of the wave. (d) Find the corresponding  $\bar{H}$  field.

(Sol.) Phasor: 
$$\vec{E} = \hat{x} 2e^{-jz/\sqrt{3}} + \hat{y}ie^{-jz/\sqrt{3}}$$

(a) 
$$\omega = 10^8 \Rightarrow f = 1.59 \times 10^7 \, Hz$$
,  $k = \frac{1}{\sqrt{3}} \Rightarrow \lambda = \frac{2\pi}{k} = 2\sqrt{3}\pi$ 

(b) 
$$v = \frac{\omega}{\beta} = \sqrt{3} \times 10^8 = 1/\sqrt{\mu_0 \varepsilon_0 \varepsilon_r} \Rightarrow \varepsilon_r = 3$$

(c) It is the left–hand elliptically-polarized wave propagating along +z direction.

(d) 
$$\eta = \sqrt{\frac{\mu_0}{\varepsilon_0 \varepsilon_r}} = \frac{120\pi}{\sqrt{3}}, \ \hat{a}_n = \hat{z}$$

$$\vec{H} = \frac{1}{\eta} \hat{a}_n \times \vec{E} = \frac{1}{\eta} \hat{z} \times (\hat{x} 2e^{-jz/\sqrt{3}} + \hat{y} j e^{-jz/\sqrt{3}}) = \frac{\sqrt{3}}{120 \pi} (\hat{y} 2e^{-jz/\sqrt{3}} - \hat{x} j e^{-jz/\sqrt{3}})$$

$$\Rightarrow \vec{H}(z,t) = \text{Re}[\vec{H}(z)e^{j\omega t}] = \frac{\sqrt{3}}{120\pi} [\hat{x}\sin(10^8 t - \frac{z}{\sqrt{3}}) + \hat{y}2\cos(10^8 t - \frac{z}{\sqrt{3}})]$$

Eg. Write down the instantaneous expression for the electric- and magnetic-field intensities of sinusoidal time-varying uniform plane wave propagating in free space and having the following characteristics: (1) f=10GHz; (2) direction of propagation is the +z direction; (3) left-hand circular polarization; (4) the initial condition is the electric field in the z=0 plane and t=0 having an x-component equal to  $E_0$  and a  $E_0$ -component equal to  $E_0$ -compo

(Sol.) 
$$\omega = 2\pi \times 10^{10}$$
,  $v = \frac{\omega}{k} = c = 3 \times 10^{8} \Rightarrow k = \frac{2\pi}{3} \times 10^{2}$   
Phasor:  $\vec{E} = \hat{x}Ae^{-j(kz+\theta)} + \hat{y}jAe^{-j(kz+\theta)}$  for the left-hand circular polarization  $\Rightarrow \vec{E}(z,t) = \text{Re}\left\{\hat{x}Ae^{-(jkz+\theta)} + \hat{y}jAe^{-j(kz+\theta)}\right\}e^{j\omega t}\right\} = \hat{x}A\cos(\omega t - kz + \theta) - \hat{y}A\sin(\omega t - kz + \theta)$ 
 $z = 0 \text{ and } t = 0$ ,  $\vec{E}(0,0) = \hat{x}A\cos(\theta) - \hat{y}A\sin(\theta) = \hat{x}E_0 + \hat{y}\sqrt{3}E_0 \Rightarrow \theta = \tan^{-1}(-\sqrt{3}), A = 2E_0$ 

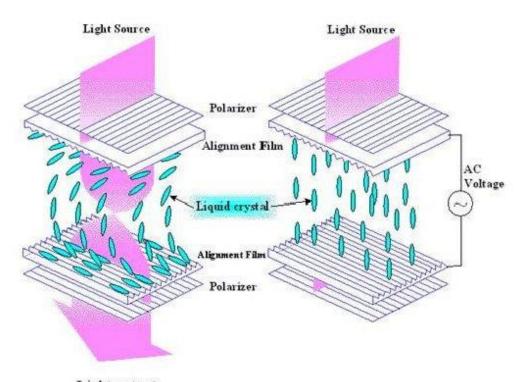
$$\vec{E}(z,t) = \hat{x}2E_0\cos[2\pi 10^{10}t - \frac{2\pi}{3}10^2z + \tan^{-1}(-\sqrt{3})] - \hat{y}2E_0\sin(2\pi 10^{10}t - \frac{2\pi}{3}10^2z + \tan^{-1}(-\sqrt{3})]$$

$$\vec{H} = \frac{1}{\eta_0}\hat{a}_n \times \vec{E} = \frac{1}{\eta_0}\hat{z} \times [\hat{x}Ae^{-j(kz+\theta)} - \hat{y}jAe^{-j(kz+\theta)}] = \frac{2E_0}{120\pi}[\hat{y}e^{-j(kz+\theta)} + \hat{x}je^{-j(kz+\theta)}]$$

$$\Rightarrow \vec{H}(z,t) = \text{Re}[\vec{H}(z)e^{j\omega t}]$$

### Application of polarization: Liquid Crystal Display (LCD)

The polarizations of incident lights are synchronized by the rotations of molecules of liquid crystal, which were controlled by an AC voltage. And then the output polarizer can block the orthogonally-polarized lights to control the output optical intensities.



Light output

# **Poynting vector:** $\vec{P} = \vec{E} \times \vec{H}$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}, \quad \nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \quad \Rightarrow \nabla \cdot (\vec{E} \times \vec{H}) = \vec{H} \cdot (\nabla \times \vec{E}) - \vec{E} \cdot (\nabla \times \vec{H}) = -\vec{H} \cdot \frac{\partial \vec{B}}{\partial t} - \vec{E} \cdot \frac{\partial \vec{D}}{\partial t} - \vec{E} \cdot \vec{J}$$

$$= -\vec{H} \cdot \frac{\partial (\mu \vec{H})}{\partial t} - \vec{E} \cdot \frac{\partial (\varepsilon \vec{E})}{\partial t} - \vec{E} \cdot \vec{J} = -\frac{\partial}{\partial t} (\frac{1}{2} \mu |\vec{H}|^2) - \frac{\partial}{\partial t} (\frac{1}{2} \varepsilon |\vec{E}|^2) - \sigma |\vec{E}|^2$$

$$\therefore \iint_{\mathcal{E}} (\vec{E} \times \vec{H}) \cdot d\vec{S} = \iiint_{\mathcal{V}} \nabla \cdot (\vec{E} \times \vec{H}) dv = -\frac{\partial}{\partial t} \iiint_{\mathcal{V}} (\frac{\mathcal{E}}{2} |\vec{E}|^2 + \frac{\mu}{2} |\vec{H}|^2) dv - \iiint_{\mathcal{V}} \sigma |\vec{E}|^2 dv$$

 $\Rightarrow \vec{P} = \vec{E} \times \vec{H}$  is the electromagnetic power flow per unit area.

**Instantaneous power density:**  $\vec{P}(z,t) = \text{Re}[\vec{E}(z)e^{j\omega t}] \times \text{Re}[\vec{H}(z)e^{j\omega t}]$ 

$$\text{Set} \quad \vec{E}(z) = \hat{x}E_x(z) = \hat{x}E_0e^{-(\alpha+j\beta)z} \\ \Rightarrow \vec{H}(z) = \frac{1}{\eta}[\hat{a}_n \times \vec{E}(z)] = \hat{y}\frac{E_0}{|\eta|}e^{-\alpha z} \cdot e^{-j(\beta z + \theta_\eta)},$$

$$\vec{E}(z,t) = \text{Re}[\vec{E}(z)e^{j\omega t}] = \hat{x}E_0e^{-\alpha z}\cos(\omega t - \beta z)$$

and 
$$\vec{H}(z,t) = \text{Re}[H(z)e^{j\omega t}] = \hat{y}\frac{E_0}{|\eta|}e^{-\alpha z}\cos(\omega t - \beta z - \theta_{\eta})$$

$$\Rightarrow \vec{P}(z,t) = \vec{E}(z,t) \times \vec{H}(z,t) = \text{Re}[\vec{E}(z)e^{j\omega t}] \times \text{Re}[\vec{H}(z)e^{j\omega t}]$$

$$=\hat{z}\frac{\left|E_{0}\right|^{2}}{2|\eta|}e^{-2\alpha z}\left[\cos\theta_{\eta}+\cos(2\omega t-2\beta z-\theta_{\eta})\right]\propto\left|E_{0}\right|^{2}$$

Average power density:  $\vec{P}_{av} = \frac{1}{2} \operatorname{Re}(\vec{E} \times \vec{H}^*)$ 

$$\vec{P}_{av} = \frac{1}{T} \int_0^T \vec{P}(z,t) dt = \hat{z} \frac{\left|E_0\right|^2}{2|\eta|} e^{-2\alpha z} \cos \theta_{\eta}$$
, where  $T$  is the period. And it can be proved that

$$\vec{P}_{av} = \frac{1}{2} \operatorname{Re}(\vec{E} \times \vec{H}^*)$$
.

Eg. Show that  $\vec{P}(z,t)$  of a circularly–polarized plane wave propagating in a lossless medium is a constant.

(Sol.) Assuming right—hand circularly—polarized plane wave,  $\hat{a}_n = \hat{z}$ 

$$\vec{E}(z,t) = E_0[\hat{x}\cos(\omega t - \beta z) + \hat{y}\sin(\omega t - \beta z)]$$

$$\vec{H}(z,t) = \frac{1}{\eta}(\hat{a}_n \times \vec{E}) = \frac{E_0}{\eta}[-\hat{x}\sin(\omega t - \beta z) + \hat{y}\cos(\omega t - \beta z)]$$

$$\vec{P}(z,t) = \vec{E}(z,t) \times \vec{H}(z,t) = \hat{z} \frac{{E_0}^2}{n}$$

Eg. Find  $\bar{P}$  on the surface of a long, straight conducting wire of radius b and conductivity  $\sigma$  that carries a direct current I. Verify Poynting's theorem.

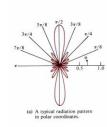
(Sol.) 
$$\vec{J} = \hat{z} \frac{I}{\pi b^2} \Rightarrow \vec{E} = \frac{\vec{J}}{\sigma} = \hat{z} \frac{I}{\sigma \pi b^2}, \quad \vec{H} = \hat{a}_{\phi} \frac{I}{2\pi b} \Rightarrow \vec{P} = \vec{E} \times \vec{H} = -\hat{a}_r \frac{I^2}{2\sigma \pi^2 b^3}$$

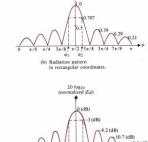
$$- \iint_{s} \vec{P} \cdot d\vec{S} = - \iint_{s} \vec{P} \cdot \hat{a}_{r} dS = \frac{I^{2}}{2\sigma\pi^{2}b^{2}} \cdot 2\pi b\ell = I^{2}(\frac{\ell}{\sigma\pi b^{2}}) = I^{2}R$$

#### **Radiation Patterns of Antennas:**

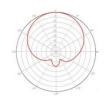
**Half-power beam width:** Angular width of main beam between the half-power (-3dB) points

**Sidelobe level:** ( $|E_{\text{max}}|$  in one sidelobe)/( $|E_{\text{max}}|$  in main beam) **Null positions:** Directions which have no radiations in the far-field zone.





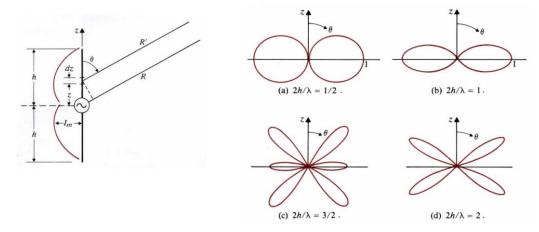
Note: The half-power beam width of the antenna for broadcasting or wireless communication is wide but its directivity is low. Contrarily, the half-power beam width of the Radar antenna for detecting targets is narrow but its directivity is high.





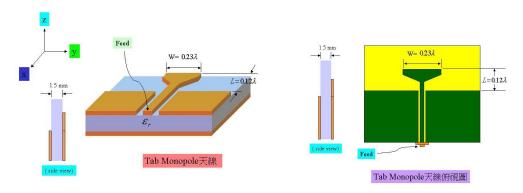
Antenna for broadcasting or wireless communication

#### **Radiation patterns of linear dipoles:**

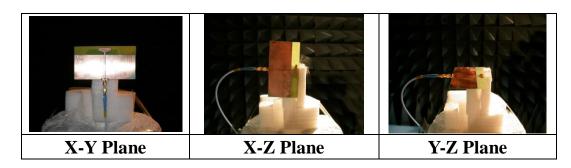


E-plane radiation patterns for center-fed dipole antennas

# **Some examples of coplanar antennas** (by H. –C. Chen and Dr. I-Fong Chen):





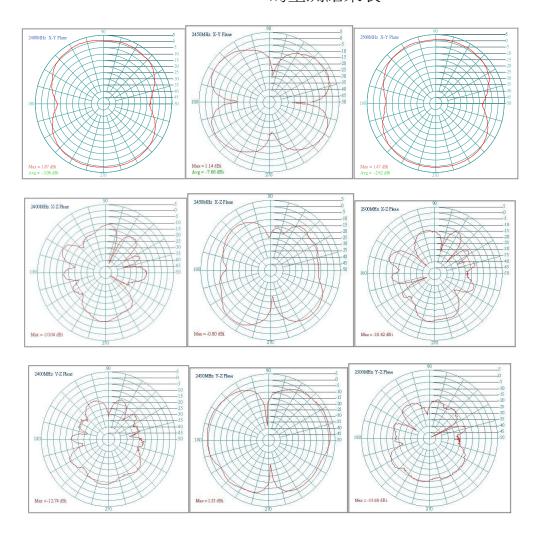


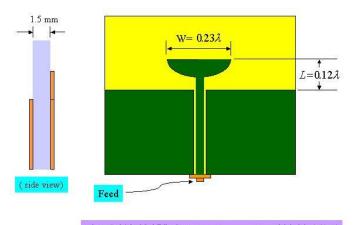
Test Result

Freq.	X-Y Plane		X-Z Plane		Y-Z Plane	
(MHz)	Vertical	Horizontal	Vertical	Horizontal	Vertical	Horizontal
2400	1.87	1.71	-10.04	-0.42	-12.74	2.26
2450	1.66	1.14	-10.00	-0.80	-13.37	1.55
2500	1.47	0.88	-10.42	-0.09	-13.68	1.93

Unit: dBi

# 2.4G~2.5GHz 的量測結果表





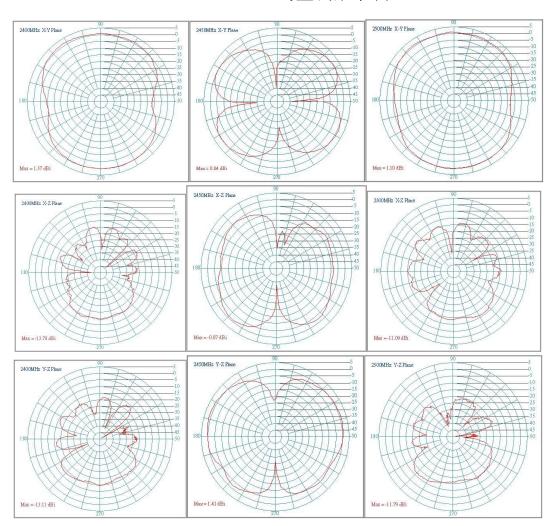
半圓型輻射體之Tab Monopole天線俯視圖

Test Result

Freq. (MHz)	X-Y Plane		X-Z Plane		Y-Z Plane	
	Vertical	Horizontal	Vertical	Horizontal	Vertical	Horizontal
2400	1.57	1.30	-13.78	-0.76	-13.11	1.81
2450	1.24	0.84	-12.96	-0.87	-10.89	1.41
2500	1.10	1.31	-11.09	-0.43	-11.79	0.86

Unit: dBi

2.4G~2.5GHz 的量測結果表



**Phased Array:**  $:: \cos \phi_0 = \frac{-\xi}{\beta d}$ ,  $:: \text{Vary } \xi \text{ electrically} \Rightarrow \text{Vary } \varphi_0 \text{ (the direction of the direction)}$ 

main beam). It can be utilized as a military radar system to scan and track a target.



#### 2-6 Plane EM Wave in a Lossy Media

$$\nabla \times H = \vec{J} + j\omega\varepsilon\vec{E} = \sigma\vec{E} + j\omega\varepsilon\vec{E} = j\omega(\varepsilon - j\frac{\sigma}{\omega})\vec{E} = j\omega\varepsilon_c\vec{E}, \varepsilon_c = \varepsilon - j\frac{\sigma}{\omega} = \varepsilon' - j\varepsilon''.$$

Complex wave number: 
$$k_c = \omega \sqrt{\mu \varepsilon_c}$$
. Loss tangent:  $\tan \delta_c \approx \varepsilon'' / \varepsilon' = \frac{\sigma}{\omega \varepsilon}$ 

**Propagation constant:** 
$$\gamma = jk_c = j\omega\sqrt{\mu\varepsilon_c} = \alpha + j\beta = j\omega\sqrt{\mu\varepsilon}\left(1 + \frac{\sigma}{j\omega\varepsilon}\right)^{1/2}$$

$$E \propto e^{-\gamma z} = e^{-jk_c z} = e^{-\alpha z} \cdot e^{-j\beta z}$$

If the medium is lossless $\rightarrow \alpha=0$  and  $k_c=\beta$ ; else if the medium is lossy $\rightarrow \alpha>0$ .

**Phase constant:** 
$$\beta = \frac{2\pi}{\lambda}$$

$$\Rightarrow \alpha = \omega \sqrt{\frac{\mu \varepsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} - 1 \right]^{\frac{1}{2}}, \quad \beta = \omega \sqrt{\frac{\mu \varepsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega \varepsilon}\right)^2} + 1 \right]^{\frac{1}{2}}$$

Case 1 Low-loss Dielectric: 
$$\frac{\sigma}{\omega \varepsilon} \ll 1 \Rightarrow \alpha \approx \frac{\sigma}{2} \sqrt{\frac{\mu}{\varepsilon}}, \quad \beta \approx \omega \sqrt{\mu \varepsilon} \left[ (1 + \frac{1}{8} (\frac{\sigma}{\omega \varepsilon})^2) \right]$$

Intrinsic impedance: 
$$\eta_c \approx \sqrt{\frac{\mu}{\varepsilon}} (1 + j \frac{\sigma}{2\omega\varepsilon})$$

Phase velocity: 
$$v_p = \frac{\omega}{\beta} = \frac{1}{\sqrt{\mu\varepsilon_c}} \approx \frac{1}{\sqrt{\mu\varepsilon}} [1 - \frac{1}{8} (\frac{\sigma}{\omega\varepsilon})^2]$$

Case 2 Good Conductor: 
$$\frac{\sigma}{\omega \varepsilon} >> 1 \Rightarrow \alpha = \beta \approx \sqrt{\frac{\omega \mu \sigma}{2}} = \sqrt{\pi f \mu \sigma}$$
,

and 
$$\eta_c = \sqrt{\frac{\mu}{\varepsilon_c}} \approx (1+j)\sqrt{\frac{\pi f \mu}{\sigma}} = (1+j)\frac{\alpha}{\sigma}$$
 Phase velocity:  $v_p = \frac{\omega}{\beta} \approx \sqrt{\frac{2\omega}{\mu\sigma}}$ 

**Skin Depth (depth of penetration):** 
$$\delta = \frac{1}{\alpha} = \frac{1}{\sqrt{\pi f \mu \sigma}}$$
.

For a good conductor, 
$$\delta = \frac{1}{\alpha} \approx \frac{1}{\beta} = \frac{\lambda}{2\pi}$$

Eg.  $\vec{E}(t,z) = \hat{x}100\cos(10^7 \pi t) \, V/m$  at z=0 in seawater:  $\varepsilon_r=72$ ,  $\mu_r=1$ ,  $\sigma=4S/m$ . (a) Determine  $\alpha$ ,  $\beta$ ,  $\nu_p$ , and  $\eta_c$ . (b) Find the distance at which the amplitude of E is 1% of its value at z=0. (c) Write E(z,t) and H(z,t) at z=0.8m, suppose it propagates in the +z direction.

(Sol.)  $\omega = 10^7 \pi$ ,  $f=5 \times 10^6 Hz$ ,  $\sigma/\omega \varepsilon_0 \varepsilon_r = 200 >> 1$ ,  $\therefore$  Seawater is a good conductor in this case.

(a) 
$$\alpha = \sqrt{\pi f \mu \sigma} = 8.89 Np/m = \beta$$
,  $\eta_c = (1+j)\sqrt{\frac{\pi f \mu}{\sigma}}$ 

$$v_p = \frac{\omega}{\beta} = 3.53 \times 10^6 \, m/s$$
,  $\lambda = \frac{2\pi}{\beta} = 0.707 \, m$ ,  $\delta = \frac{1}{\alpha} = 0.112 \, m$ 

(b) 
$$e^{-\alpha z} = 0.01 \Rightarrow z = \frac{1}{\alpha} \ln(100) = 0.518 m$$

(c) 
$$E(z,t) = \text{Re}[E(z)e^{j\omega t}] = \hat{x}100e^{-\alpha z}\cos(\omega t - \beta z)$$

$$z = 0.8m \Rightarrow E(0.8,t) = \hat{x}100e^{-0.8\alpha}\cos(\omega t - 0.8\beta) = \hat{x}0.082\cos(10^7 \pi t - 7.11)$$

$$\vec{H}(0.8,t) = \frac{1}{\eta} \hat{a}_n \times \vec{E}(0.8,t), \quad H(0.8,t) = \hat{y} \operatorname{Re}\left[\frac{E_x(0.8)}{\eta_c} e^{j\omega t}\right] = \hat{y} 0.026 \cos(10^7 \pi t - 1.61)$$

Eg. The magnetic field intensity of a linearly polarized uniform plane wave propagating in the +y direction in seawater  $\varepsilon_r$ =80,  $\mu_r$ =1,  $\sigma$ =4S/m is

$$\vec{H} = \hat{x}0.1\sin(10^{10}\pi t - \frac{\pi}{3})$$
 A/m. (a) Determine the attenuation constant, the phase

constant, the intrinsic impedance, the phase velocity, the wavelength, and the skin depth. (b) Find the location at which the amplitude of H is 0.01 A/m. (c) Write the expressions for E(y,t) and H(y,t) at y=0.5m as function of t.

(Sol.) (a)  $\sigma/\omega\varepsilon=0.18<<1$ ,  $\therefore$  Seawater is a low-loss dielectric in this case.

$$\Rightarrow \alpha \approx \frac{\sigma}{2} \sqrt{\frac{\mu}{\varepsilon}} = 83.96 Np/m \qquad \eta_c \approx \sqrt{\frac{\mu}{\varepsilon}} (1 + j \frac{\sigma}{2\omega \varepsilon}) = 41.8 e^{j0.0283\pi}$$

$$\beta \approx \omega \sqrt{\mu \varepsilon} \left[ (1 + \frac{1}{8} (\frac{\sigma}{\omega \varepsilon})^2) \right] = 300 \pi , \quad v_p = \frac{\omega}{\beta} = 3.33 \times 10^7 m/s , \quad \delta = \frac{1}{\alpha} = 1.19 \times 10^{-2} m ,$$

$$\lambda = \frac{2\pi}{\beta} = 6.67 \times 10^{-3} \, m$$

(b) 
$$e^{-\alpha y} = \frac{0.01}{0.1} \Rightarrow y = \frac{1}{\alpha} \ln 10 = 2.74 \times 10^{-2} m$$

(c) 
$$H(y,t) = \hat{x}0.1e^{-\alpha y} \sin(10^{10}\pi t - \beta y - \frac{\pi}{3}), \quad y = 0.5, \beta = 300\pi$$

$$\Rightarrow \vec{H}(0.5,t) = \hat{x}5.75 \times 10^{-20} \sin(10^{10} \pi t - \frac{\pi}{3})$$

$$\hat{a}_n = \hat{y} \Rightarrow \vec{E}(0.5, t) = -\eta_c \hat{a}_n \times \vec{H}(0.5, t) = \hat{z}2.41 \times 10^{-18} \sin(10^{10}\pi t - \frac{\pi}{3} + 0.0283\pi)$$

Eg. Given that the skin depth for graphite at  $100 \ MHz$  is 0.16mm, determine (a) the conductivity of graphite, and (b) the distance that a 1GHz wave travels in graphite such that its field intensity is reduced by 30dB.

(Sol.) (a) 
$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}} = 0.16 \times 10^{-3} \Rightarrow \sigma = 0.99 \times 10^{5} \, \text{S/m}$$

(b) At 
$$f=10^9 Hz$$
,  $\alpha = \sqrt{\pi f \mu \sigma} = 1.98 \times 10^4 Np/m$ 

$$-30(dB) = 20\log_{10}e^{-\alpha z} \Rightarrow z = \frac{1.5}{\alpha\log_{10}e} = 1.75 \times 10^{-4} m$$

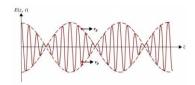
Eg. Determine and compare the intrinsic impedance, attenuation constant, and skin depth of copper  $\sigma_{cu}=5.8\times10^7 S/m$ , silver  $\sigma_{ag}=6.15\times10^7 S/m$ , and brass  $\sigma_{br}=1.59\times10^7 S/m$  at following frequencies: 60Hz and 1GHz.

(Sol.) 
$$\alpha = \sqrt{\pi f \mu \sigma}$$
,  $\delta = \frac{1}{\alpha}$ ,  $f \uparrow \Rightarrow \delta \downarrow$ ,  $\eta_c = (1+j)\frac{\alpha}{\sigma}$ 

Copper: 
$$60Hz \Rightarrow \eta_c = 2.02(1+j) \times 10^{-6} \Omega$$
,  $\alpha = 1.17 \times 10^2 Np/m$ ,  $\delta = 8.53 \times 10^{-3} m$ 

$$1GHz \Rightarrow \eta_c = 8.25(1+j) \times 10^{-3} \Omega$$
,  $\alpha = 4.79 \times 10^5 Np/m$ ,  $\delta = 2.09 \times 10^{-6} m$ 

Group velocity: 
$$v_g = \frac{d\omega}{d\beta} = \frac{1}{d\beta/d\omega}$$



$$\begin{split} \vec{E}(t,z) &= E_0 \cos[(\omega + \Delta \omega)t - (\beta + \Delta \beta)z] + E_0 \cos[(\omega - \Delta \omega)t - (\beta - \Delta \beta)z] \\ &= 2E_0 \cos(t\Delta \omega - z\Delta \beta)\cos(\omega t - \beta z) \end{split}$$

Let 
$$t\Delta\omega - z\Delta\beta = \text{constant} \implies v_g = \frac{dz}{dt} = \frac{\Delta\omega}{\Delta\beta} = \frac{1}{\Delta\beta/\Delta\omega} = \frac{d\omega}{d\beta} = \frac{1}{d\beta/d\omega}$$

Eg. Show that 
$$v_g = v_p + \beta \frac{dv_p}{d\beta}$$
 and  $v_g = v_p - \lambda \frac{dv_p}{d\lambda}$ 

(Proof) 
$$v_p = \frac{\omega}{\beta}$$
,  $\omega = v_p \beta$ ,  $v_g = \frac{d\omega}{d\beta} = v_p + \beta \frac{dv_p}{d\beta}$ 

$$\therefore \beta = \frac{2\pi}{\lambda}, \quad \beta\lambda = 2\pi, \quad \lambda d\beta + \beta d\lambda = 0 \Rightarrow \frac{\beta}{d\beta} = -\frac{\lambda}{d\lambda}, \quad v_g = v_p - \lambda \frac{dv_p}{d\lambda}$$

An example of longitudinal  $v_p>0$  but longitudinal  $v_g=0$  in barber's pole.



Plasma: Ionized gasses with equal electron and ion densities.

**Ionosphere:** 50~500 *Km* in altitude

**Simple model of plasma:** An electron of charge -e, mass m, position  $\vec{x}$ 

$$-e\vec{E} = m\frac{d^2\vec{x}}{dt^2} = -m\omega^2\vec{x} \Rightarrow \vec{x} = \frac{e}{m\omega^2}\vec{E} \Rightarrow \text{Electric dipole} \quad \vec{p} = -e\vec{x} = \frac{-e^2}{m\omega^2}\vec{E}$$

... Total electric dipole moment:  $\vec{P} = N\vec{p} = -\frac{Ne^2}{m\omega^2}\vec{E}$ 

$$\vec{D} = \varepsilon_0 \vec{E} + \vec{P} = \varepsilon_0 (1 - \frac{Ne^2}{m\omega^2 \varepsilon_0}) \vec{E} = \varepsilon_0 (1 - \frac{\omega_p^2}{\omega^2}) \vec{E}, \text{ where } \omega_p = \sqrt{\frac{Ne^2}{m\varepsilon_0}} \text{ is the plasma}$$

angular frequency, and the effective permittivity is  $\varepsilon = \varepsilon_0 (1 - \frac{{\omega_p}^2}{\omega^2}) = \varepsilon_0 (1 - \frac{{f_p}^2}{f^2})$ .

Propagation constant: 
$$\gamma = j\omega\sqrt{\mu\varepsilon_0} \cdot \sqrt{1 - (\frac{f_p^2}{f^2})}$$

Intrinsic impedance of the plasma: 
$$\eta_c = \frac{\eta_0}{\sqrt{1 - (\frac{f_p}{f})^2}}$$
 where  $\eta_0 = 120 \pi(\Omega)$ 

Case  $1 f < f_p$ :  $\gamma$  is real,  $\eta_c$  is pure imaginary  $\Rightarrow$  Attenuation  $\Rightarrow$  EM wave is in cutoff. Case  $2 f > f_p$ :  $\gamma$  is pure imaginary,  $\eta_c$  is real  $\Rightarrow$  EM wave can propagate through the plasma.